

Stress Analysis of Highly Jointed Rock Using Parallel Processing

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Abstract:

Computational stress analysis is now widely used in geomechanics for back analysis of observed rock mass behaviour around surface and underground excavations and as a tool for excavation design in mining and civil engineering. The distinct element (DE) method, represents a rock mass as a discontinuum, and has been shown to be more realistic than finite element (FE) or boundary element (BE) (continuum) methods for modelling systems such as subsiding strata over underground coal mine excavations. In this initial study a DE code been implemented in the applicative parallel processing language SISAL, explicit parallel Pascal and compared with the performance of the original FORTRAN implementation The work presented here is part of a larger study into the implementation of DE methods on parallel computer systems.

1. Introduction

Computational stress analysis is now widely used in geomechanics for back analysis of observed rock mass behaviour around surface and underground excavations and as a tool for excavation design in mining and civil engineering. The distinct element (DE) method, which represents a rock mass as a discontinuum, has been shown to be more realistic than finite element (FE) or boundary element (BE) (continuum) methods for modelling systems such as subsiding strata over underground coal mine excavations. However, whereas even 3D FE and BE analyses can now be performed readily on engineering workstations or the more powerful personal computers, the DE method generally requires orders of magnitude more computer processing time for analyses of comparable complexity. This has so far prevented the DE method from being applied widely in excavation design in industry.

Most DE codes are based upon an explicit time integration of Newton's laws of motion for each DE, usually involving many thousands of time steps or solution cycles in a full analysis. The explicit numerical method implies that, within each cycle, calculations for each DE can be carried out in parallel. With the growing availability of moderately priced medium range multiprocessors, multiprocessor workstations and parallel language systems there is the potential to obtain satisfactory performance at a reasonable cost.

In this paper we develop parallel processing versions of a relatively simple 2D DE stress analysis code. This code, originally implemented in FORTRAN, has been implemented in SISAL a modern applicative language, and Pascal an imperative language.

The changes made to the program and its translation into SISAL and Pascal will be outlined, times for the original SISAL and Pascal versions reported, and some preliminary conclusions drawn regarding the usefulness of various parallel processing options for DE stress analysis codes.

2. The Distinct Element Method

The DE method of stress analysis was introduced in [1] to deal with problems in rock mechanics which could not be treated adequately by the conventional continuum methods. The earliest DE programs (e.g. program RBM in [2]) assumed that the DEs were rigid, so that all deformations within the system took place at the DE interfaces. A second program described in [2], SDEM, allowed modelling of three simple modes of deformation of each DE - two compressive and one shear mode. The DE programs which are most widely used at present are UDEC [3] and 3DEC [4]; the DEs in each of these may be modelled as fully deformable via internal finite difference zoning.

2.1 Theoretical basis

Most DE programs are based on force-displacement relations describing DE interactions and Newton's second law of motion for the response of each DE to the unbalanced forces and moments acting on it.

The normal forces developed at a point of contact between DEs are calculated from the notional overlap of those DEs and the specified normal stiffness of the inter-DE joints. Tensile normal forces are usually not permitted, i.e. there is no restraint placed upon opening of a contact between DEs.

Shear interactions are load-path dependent, so incremental shear forces are calculated from the increments in shear displacement, in terms of the shear stiffness of the joints. The maximum shear force is usually limited by a Mohr-Coulomb or similar strength criterion.

The motion of each DE under the action of gravity, external loadings and the forces arising from contact with other DEs is determined from Newton's second law. A damping mechanism is also included in the model to account for dissipation of vibrational energy in the system.

The equations of motion may be integrated with respect to time using a central difference scheme to yield velocities and then integrated again to yield displacements. The velocity dependent damping terms have been omitted here for simplicity, but the same form of equations hold even when damping is included.

$$u'_i(t+\Delta t) = u'_i(t) + (\sum F_i(t)/m + g_i) \cdot \Delta t \quad (1)$$

$$u_i(t+\Delta t) = u_i(t-\Delta t) + u'_i(t+\Delta t) \cdot \Delta t \quad (2)$$

where $i = 1, 2$ correspond to x and y directions respectively;
 u_i are the components of displacement of the DE centroid;
 F_i are the components of non-gravitational forces acting on the DE;
 g_i are the components of gravitational acceleration;
 m is the mass of the particular DE.

The equation of rotation for each DE can be integrated similarly. Note that, in the integrated equations, DE velocities and displacements are expressed explicitly in term of values at a previous time and so may each be calculated independently.

The calculation cycle proceeds, with the calculated displacements being used to update the geometry of the system, and thence to determine new DE interaction forces. These, in turn, are used in the next stage of the explicit integration of Newton's equations.

This explicit time integration scheme is only conditionally stable. Physically, the time step must be small enough that information cannot pass between neighbouring DEs in one step, thus justifying the independence of the integrated equations of motion.

2.2 DECYL

DECYL is a simple program which analyses 2 dimensional systems of interacting, rigid circular DEs of equal radius [5]. It is based on the same explicit integration algorithm used in DE programs for practical stress analysis of highly jointed rock. DECYL assumes that any of the circular DEs comprising the system being modelled may be in contact with any other DE; contact lists are not maintained and physical locality is not exploited. The diagrammatic representation of a DECYL system is shown in Figure 1. The general flow of computation in DECYL is shown in Figure 2.

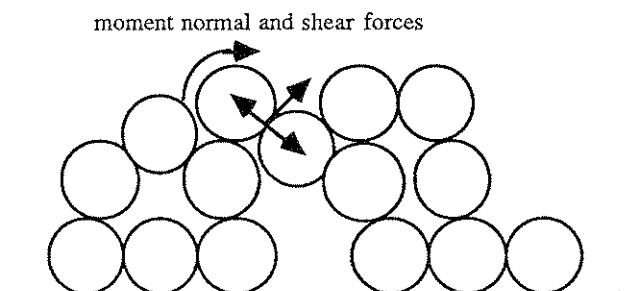


Figure 1. a DECYL system

```

while not stable do
  for j in 1 to no_DEs+1 do
    for i in j+1 to no_DEs+1 do
      if touching DE[i] and DE[j] then
        compute normal force
        if normal force > 0 then
          compute moment
          compute shear force
          if slipping then
            adjust shear force
          resolve force components
          accumulate forces and moments acting on DE[j] and DE[i]

    integrate accelerations on DE[j]
    compute new position of DE[j]

```

Figure 2. DECYL computational flow

3. Machines and languages

3.1 Machines

The machines used in this study were two Encore Multimax multiprocessor (one with four XPC processors at ~4MIP each and the other with 20 slower APC processors at ~2MIP each), an IBM RS6000/530 uniprocessor workstation and a Cray YMP. The IBM workstation was chosen as its CPU performance will be representative of CPUs in future medium cost multiprocessors. The Cray YMP single processor performance provides a reference point.

3.2 Languages

The languages used in the study were SISAL, explicit parallel Pascal and, as a language reference point, sequential FORTRAN.

SISAL [9] is an applicative language which has been targetted at a wide variety of systems including uniprocessors, current generation multiprocessors such as the Encore Multimax and research dataflow machines [10][11][12]. The textual form of SISAL, in terms of control structures and array representations, (Appendix) provides a relatively easy transition for those familiar with imperative languages and the optimising SISAL compiler (osc) from Colorado has yielded performance competitive with FORTRAN [13][14]. SISAL requires no directives or annotation at the source level.

The SISAL compiler exploits loop concurrency. Loops with no dependencies between cycles are 'sliced' into several loops each over some some number of cycles of the original loop. The number of slices is determined at runtime with the slices being executed concurrently.

For the Pascal implementation we used the standard UNIX fork primitive and the parallel programming primitives available in the Encore Multimax.

5. Results

The system used for the studies was a stack of 500 DEs for ten iterations. A 'movie' of a smaller system of 100 DEs over 8000 iterations is shown in Figure 3.

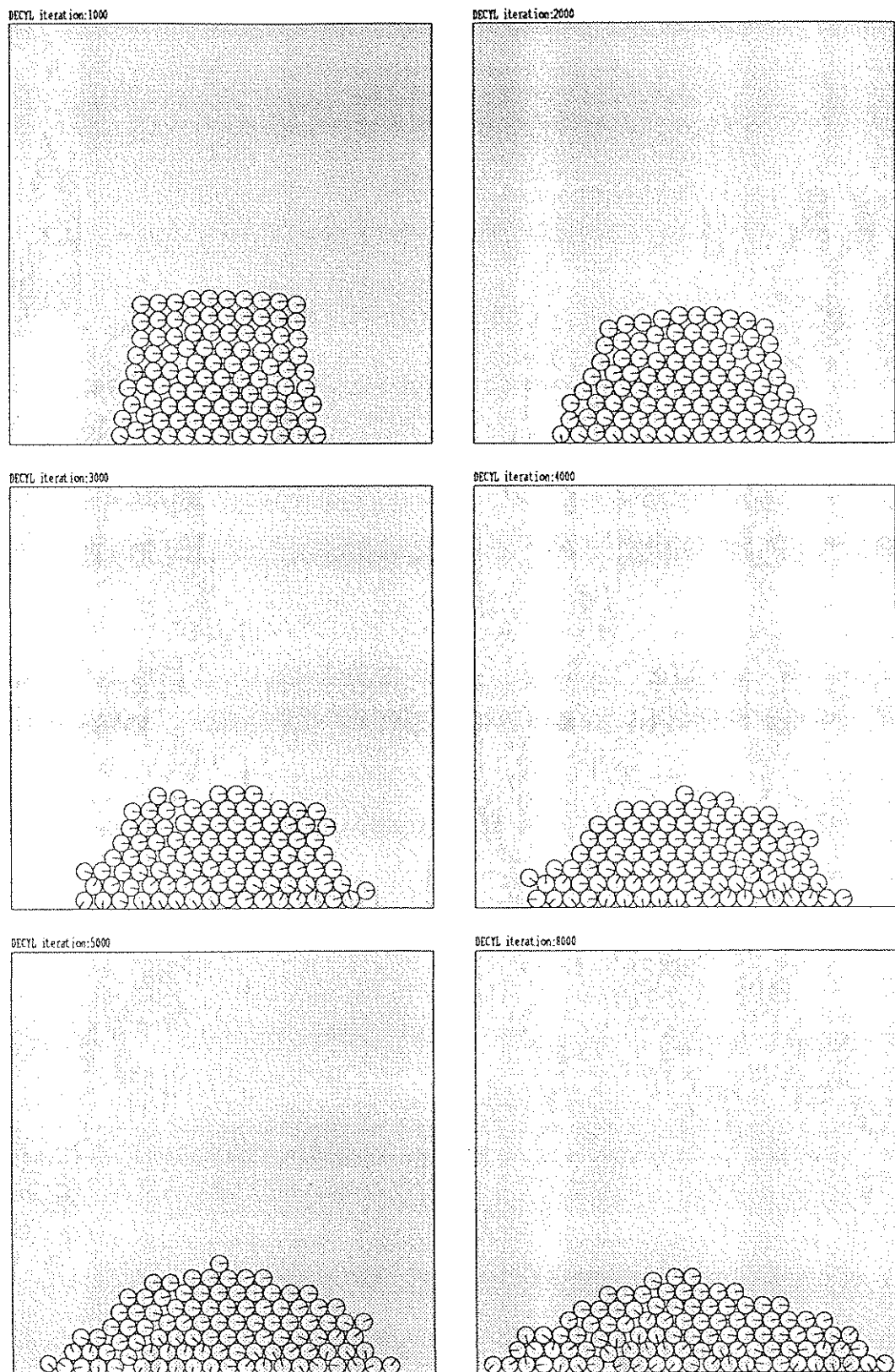


Figure 3. DECYL Movie

5.1 FORTRAN

Some elementary optimisations were performed on the FORTRAN including the elimination of division operations (Appendix A). The times (user+system) for unoptimised and optimised FORTRAN versions on the Encore Multimax and RS6000 are shown in table 1. These optimisations were carried over to the SISAL and Pascal versions. The run times for FORTRAN are used for reference against the SISAL and Pascal results which follow.

System	Compiler	original	optimised	difference
Encore Multimax (XPC)	f77 -O	73.8	31.3	-58%
IBM RS6000/530	xl f-O	6.9	4.3	-38%

Table 1. unoptimised and optimised FORTRAN times

5.2 SISAL

DECYL was translated into SISAL (Appendix B). No particular difficulty was encountered in this process as the original formulation in FORTRAN was well written with no side effects through COMMON and EQUIVALENCE statements. These FORTRAN statements can cause significant difficulties when recasting FORTRAN application codes into SISAL [16]. The speedup obtained for SISAL is presented in Figure 4.

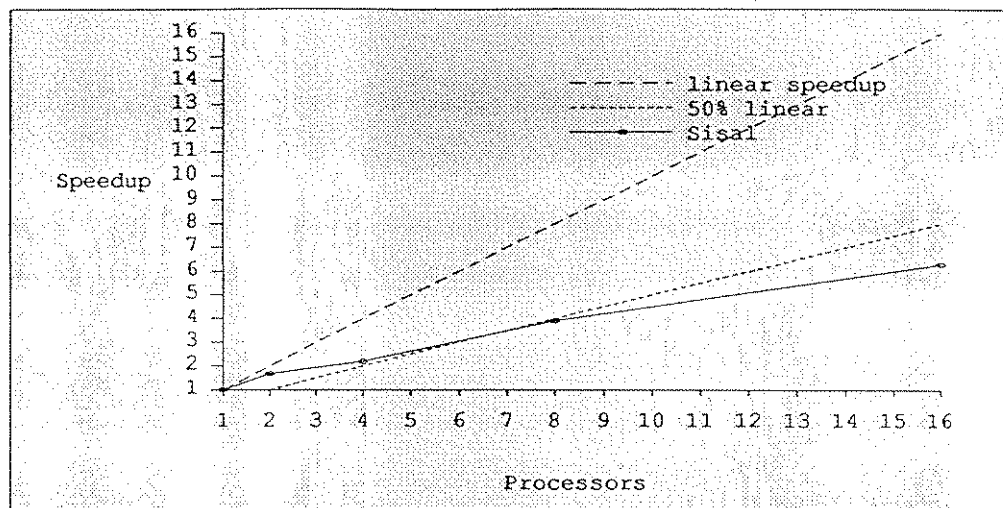


Figure 4. Speedup of DECYL in SISAL (Encore)

Further improvement in SISAL performance is expected, reducing overheads due mainly to the array construction and access mechanisms of the current implementation of SISAL. SISAL permits structures to change size at runtime involving indirect access to matrix elements via a vector of pointers to each matrix row. There are also consequential memory allocation overheads as structures are progressively constructed. The potential gains from static allocation of structures have been acknowledged by the developers of SISAL and will be seen in later SISAL versions [15].

5.2 Pascal

To amortise the startup cost of loop slices it is best to maximise the work done for each slice. The strategy then is to parallelise outer loops where possible; inner loops need only be parallelised if the bounds of the outer loop are such as to not provide sufficient slices to load the machine.

The speedup for DECYL with the inner loop annotated explicitly (appendix C) is shown in Figure 5a and with the outer loop annotated (appendix D) in Figure 5b.

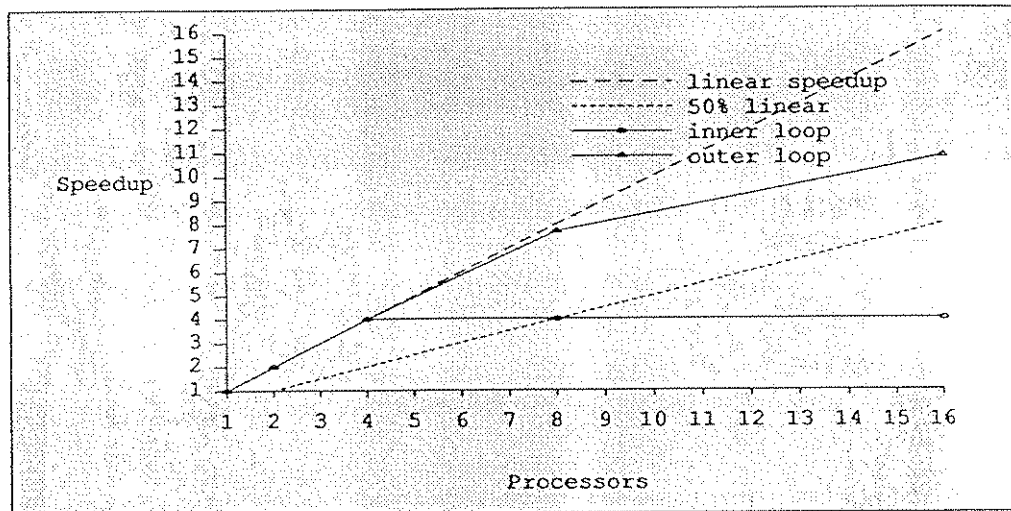


Figure 5. Speedup of DECYL in Pascal (Encore)

The collected times for SISAL, Pascal and FORTRAN on the YMP, IBM RS6000 and faster four processor Encore Multimax are given in table 2a and times for the slower Encore in table 2b.

	YMP 1 cpu	User + Sytem (seconds) speedup in ()		
		RS6000/530	Encore (XPC) 1 cpu	Encore (XPC) 4 cpus
FORTRAN	0.52	4.25	31.3	-
Sisal	5.15	11.78	57.9	25.7 (2.3)
Pascal <i>seq</i>	4.66	2.02	34.0	-
Pascal <i>inner</i>	-	-	40.3	23.6 (1.7)*
Pascal <i>outer</i>	-	-	34.6	9.0 (3.9)*

	YMP 1 cpu	Wallclock (seconds) speedup in ()		
		RS6000/530	Encore (XPC) cpu	Encore (XPC) 4 cpus
FORTRAN	0.956 (97%)	4.3	31.7	-
Sisal	33.4*	11.8	58.2	28.9
Pascal <i>seq</i>	34.0*	2.1	34.3	-
Pascal <i>inner</i>	-	-	40.8	26.0 (1.6)*
Pascal <i>outer</i>	-	-	34.9	11.1 (3.1)*

(a)

cpus	User + Sytem (seconds) speedup in ()							
	1	2	4	8	16			
FORTRAN	?	-	-	-	-			
Sisal	163.0	97.0 (1.68)	73.0 (2.2)	42.0 (3.9)	26.0 (6.3)			
Pascal <i>seq</i>	75.1	-	-	-	-			
Pascal <i>inner</i>	104.3	50.4 (2.0)	25.8 (4.0)	26.0 (4.0)	-			
Pascal <i>outer</i>	85.3	42.7 (2.0)	21.6 (4.0)	11.1 (7.7)	7.9 (10.8)*			

cpus	Wallclock (seconds) speedup in ()									
	1	2	4	8	16					
FORTRAN	?									
Sisal	164.18	98.24	(1.7)	74.1	(2.2)	43.3	(3.8)	26.04	(6.3)	
Pascal <i>seq</i>	75.1									
Pascal <i>inner</i>	96.9	53.2	(1.8)	29.2	(3.3)	29.9	(3.2)			
Pascal <i>outer</i>	86.7	44.3	(2.0)	23.7	(3.7)	13.7	(6.33)	11.7	(7.41)*	

* systems heavily loaded

YMP FORTRAN compiler (cf77 -Zp -Wf)

(b)

Table 1. Times and speedup () for 500 DEs and 10 time steps

6. Conclusions

This initial study has shown that it is possible to obtain good speedup on current multiprocessors. These processors have relatively poor scientific performance but it is certain that next generation processors will be greatly improved in this respect.

SISAL has performance competitive with FORTRAN and shows promise for implicit parallel programming. Its portability over a wide range of current parallel and high performance computer systems and next generation systems makes it attractive for studies in parallel programming.

Acknowledgements

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APPENDIX A: Optimised DECYL in FORTRAN

```

program decyl
c
c   This program was used by Dr. Loren Lorig at an internal workshop
c   on distinct element modelling at the Division of Geomechanics
c   in September 1985, just before he returned to the U.S. to join
c   Itasca Consulting Group, Inc., in Minneapolis
c
c   It is a very simple distinct element code, for 2-D analysis of the
c   mechanical interactions of a number of cylinders with each other
c   and a fixed horizontal plane. (2-D implies that the axes of all
c   the cylinders are parallel with each other and with the fixed
c   plane; analysis is on a perpendicular plane through the system.)
c
c   The cylinders all have the same radius and are rigid. Their
c   elastic interactions are governed by normal and shear stiffnesses
c   (which yield interaction forces according to the calculated
c   'overlap' at their points of contact). If the calculated shear
c   force exceeds the specified frictional strength, the cylinders
c   will slip at that point of contact; if a tensile normal force is
c   calculated at a contact, that contact will be 'broken', i.e.
c   assumed zero tensile strength.
c
c   The equations of motion for the system are solved by explicit
c   numerical integration, with some imposed artificial damping to
c   represent loss of energy within the system and to prevent it
c   'ringing' interminably.
c
c   In the case which is hard-coded into this version of the program,
c   two cylinders are resting on the horizontal plane, touching each
c   other. The third cylinder is dropped from a point on the plane
c   of symmetry. After about 2000 cycles, the cylinders come to
c   rest, with the third one sitting between the other two on the
c   plane.
c
c   We will amend the code shortly to input the geometrical and other
c   data, and to draw a simple plot of the system of cylinders, as
c   the job runs or at the end of an analysis.
c
c   Variables:
c   n cyl = number of cylinders
c           ('cylinder' n cyl+1 is the horizontal plane)
c   fn(i,j) = normal force between cylinders i and j
c   m(i,j)  = moment due to shear interaction between i and j
c   du(i)  = u-coordinate of centroid of cylinder i
c   dv(i)  = v-      "      "      "      "      "      "
c   da(i)  = a-angle of cylinder from starting position
c   u(i)   = u-component of velocity of      "      "
c   v(i)   = v-      "      "      "      "      "      "
c   w(i)   = angular velocity of cylinder i
c   ddu(i) = increment in u-component of displacement of cylinder i
c   ddv(i) =      "      " v-      "      "      "      "      "
c   gamma(i) =      "      " rotation of cylinder i
c   fxsum(i) = u(x)-component of total force acting on cylinder i
c   fysum(i) = v(y)-      "      "      "      "      "      "
c   msum(i) = total moment acting on cylinder i

```

```

c      Optimisation G.K. Egan
c      Laboratory for Concurrent Computing Systems
c      Swinburne Institute of Technology
c
c      rho = density
c      d = diameter of cylinders; r = radius
c      g = acceleration due to gravity
c      mu = coefficient of friction at contacts
c      mass = mass of cylinders; moi = moment of inertia
c      akn = normal stiffness at contacts; aks = shear stiffness
c      alpha = damping constant
c      tdel = time step
c
parameter (ncyl=500)
parameter (iside=100)
parameter (nn=ncyl+1)
dimension fn(nn,nn), m(nn,nn), fxsum(nn), fysum(nn), msum(nn),
.          u(nn), v(nn), w(nn), du(nn), dv(nn), gamma(nn),
.          ddu(nn), ddv(nn),
.          da(nn)
real m, msum, mass, mu, moi, rmoi, rmass
cgke
mod(i,j)= i-(i/j)*j
pi=4.*atan(1.)
rho=2000.
d=100.
rd=1.0/d
dsqr=d*d
r=d/2.
rr=2./d
g=-10.
mu=0.1
mass=rho*pi*r*r
rmass=1.0/mass
moi=mass*r*r/2.
rmoi=1.0/moi
akn=1.e9
aks=1.e9
frac=1.00
freq=0.200
alpha=2.*pi*frac*freq
tdel=2.*sqrt(mass/akn)/10.
con1=alpha*tdel/2.
r1plus1con1 = 1.0/(1.0+con1)
c
c      Initial coordinates of centroids of cylinders
c
c      centroid of (ncyc+1)th cylinder located at -r,
c      to give effect of fixed horizontal plane at v=0
cgke stack of cylinders
do 222 i=1,ncyl
    du(i)=mod(i,iside)*d
    dv(i)=(i/iside)*d+r
222 continue
du(nn)=0.0
dv(nn)=-r
c

```

```

c   Initialise forces, velocities etc.
c
  do 7 j=1,nn
  do 8 i=j+1,nn
  fn(j,i)=0.
  m(j,i)=0.
8 continue
  fxsum(j)=0.
  fysum(j)=0.
  msum(j)=0.
  u(j)=0.
  v(j)=0.
  w(j)=0.
  ddu(j)=0.
  ddv(j)=0.
  gamma(j)=0.
7 continue

c
c   Set up counters for time integration stepping
c   - maximum no. of steps = its
c   kount used to print progressive results every 50 steps
c
  its=10
  iframes =1
  ikount=its/iframes
  kount=ikount
  write(6,*)ncyl,its,iframes
c   write(6,102) alpha,mu
c 102 format(' Program decyl (L. Lorig 1985) with alpha =',f6.2,
c   .      ' and mu =',f6.2)
  do 4 n=1,its
  if(kount.eq.ikount) then
c   do 999 ii=1,ncyl
c999  write(6,*) n-1, r,du(ii),dv(ii),da(ii)
      kount=0
      endif
      kount=kount+1
c   Loop over cylinders
  do 3 j=1,ncyl
c   Place (ncyc+1)th cylinder 'opposite' jth
  du(nn)=du(j)
c   Set gamma for (ncyc+1)th so get no shear interaction between
c   jth cylinder and flat plane if former is rolling rather than
c   sliding
  gamma(nn)=-ddu(j)*rr
c   Look for interactions with cylinders with higher numbers
  k=j+1
  do 2 i=k,nn
  dudif=du(j)-du(i)
  dvdif=dv(j)-dv(i)
c   is the cylinder (i) touching cylinder (j) ?
  z=dudif*dudif+dvdif*dvdif
  if(z.le.dsqr) then
  rz=1./sqrt(z)
  dudif=dudif*rz
  dvdif=dvdif*rz
  ddudif=ddu(i)-ddu(j)

```

```

      dddif=ddv(i)-ddv(j)
c      calculate the normal force fn(j,i)
      dfn=akn*(ddvdif*dvdif+ddudif*dudif)
      fn(j,i)=fn(j,i)+dfn
      if(fn(j,i).ge.0.) then
c      calculate moment
      theta=(ddvdif*dudif-ddudif*dvdif)*rd
      dm=-aks*(gamma(j)+gamma(i)-theta)
      m(j,i)=m(j,i)+dm
c      calculate shear force
      ft=m(j,i)*rr
c      is slip occurring?
      ff=mu*fn(j,i)
      abft=abs(ft)
      if(abft.gt.ff) then
        ft=ff*ft/abft
      endif
      m(j,i)=r*ft
c      calculate force components (fx,fy)
      fx=fn(j,i)*dudif-ft*dvdif
      fy=fn(j,i)*dvdif+ft*dudif
c      forces on cylinder j
      fxsum(j)=fxsum(j)+fx
      fysum(j)=fysum(j)+fy
      msum(j)=msum(j)+m(j,i)
c      reactions back on cylinder j
      fxsum(i)=fxsum(i)-fx
      fysum(i)=fysum(i)-fy
      msum(i)=msum(i)+m(j,i)
      endif
      else
      fn(j,i)=0.
      m(j,i)=0.
      endif
2 continue
c
c      integrate accelerations to find displacements
      u(j)=(u(j)*(1.-con1)+((fxsum(j)*rmass)*tdel))*rlpluscon1
      v(j)=(v(j)*(1.-con1)+((fysum(j)*rmass+g)*tdel))*rlpluscon1
      w(j)=(w(j)*(1.-con1)+((msum(j)*rmoi)*tdel))*rlpluscon1
      ddu(j)=u(j)*tdel
      ddv(j)=v(j)*tdel
      gamma(j)=w(j)*tdel
      du(j)=du(j)+ddu(j)
      dv(j)=dv(j)+ddv(j)
      da(j)=da(j)+gamma(j)
      fxsum(j)=0.
      fysum(j)=0.
      msum(j)=0.
3 continue
4 continue
      stop
      end

```

APPENDIX B: DECYL in SISAL

```
% Original program decyl by Dr. Loren Lorig in FORTRAN.
% Sisal G.K. Egan Laboratory for Concurrent Computing Systems 1990
% Swinburne Institute of Technology loosely based on a version by Warwick
% Heath.
```

```
define main
```

```
type    vector = array [real];           % Data rep. copied from orig.
type    dudv_rec = record[du, dv : real] % Just for output.
```

```
global sqrt(x: real returns real)
```

```
function main( returns array[array[dudv_rec]])
```

```
for initial
```

```
  % auto generate a stack of cylinders
  ncyl:integer := 500;
  iside:integer := 100;
  i,j:integer;
  its:integer := 10;
  n : integer := ncyl+1;
  pi : real := 3.141592654;
  rho : real := 2000.0;
  d : real := 100.0;
  dd :real := d*d;
  rd :real := 1.0/d;
  r : real := d/2.0;
  rr: real := 1.0/r;
  initialdu: vector := for i in 1,ncyl
    returns array of real(i-(i/iside)*iside)*d end for;
  initialdv: vector := for i in 1,ncyl
    returns array of real(i/iside)*d+r end for;
  g : real := -10.0;
  mu :real := 0.1;
  mass : real := rho*pi*r*r;
  rmass : real := 1.0/mass;
  moi : real := mass*r*r/2.0;
  rmoi: real := 1.0/moi;
  akn : real := 1.0e9;
  aks : real := 1.0e9;
  frac : real := 1.0;
  freq : real := 0.20;
  alpha : real := 2.0*pi*frac*freq;
  tdel : real := 2.0*sqrt(mass/akn)/10.0;
  conl : real := alpha*tdel/2.0;
  r1plusconl:real := 1.0/(1.0+conl);
```

```
fn : array[vector] :=
  for j in 1,ncyl returns array of
    for i in j+1,n
      returns array of 0.0
    end for
  end for;
m : array[vector] := fn;
```

```

u : vector := array_fill(1,ncyl,0.0);
v : vector := u;
w : vector := u;
ddu : vector := u;
ddv : vector := u;
gamma : vector := u;
du : vector := initialdu;
dv : vector := initialdv;

iter : integer := 1;
cylinders : array[dudv_rec] :=
  array_fill(1,ncyl,record dudv_rec[du:0.0;dv:0.0]);

while (iter <= its) repeat % for number of iterations

fxsumj, fysumj, msumj, fn, m := for j in 1,ncyl
  alldu : vector := array_addh(old du,old du[j]);
  alldv : vector := array_addh(old dv,-r);
  allddu : vector := array_addh(old ddu,0.0);
  allddv : vector := array_addh(old ddv,0.0);
  allgamma : vector := array_addh(old gamma,(-old ddu[j])/r);

fxsumji, fysumji, msumji, fnji, mji := for i in j+1,n
  dudif : real := alldu[j] - alldu[i];
  dvdif : real := alldv[j] - alldv[i];
  z : real := dudif*dudif + dvdif*dvdif;

% Interactions with other cylinders???
fxsumji, fysumji, msumji, fnji, mji : real :=
  if (z > dd | j = i) then
    0.0, 0.0, 0.0, 0.0, 0.0
  else
    let
      rz := 1.0/sqrt(z);
      zdudif : real := dudif*rz;
      zdvdif : real := dvdif*rz;
      ddudif : real := allddu[i] - allddu[j];
      ddvdif : real := allddv[i] - allddv[j];
      % calculate the normal force between i and j
      dfn : real := akn * (ddvdif*zdvdif + ddudif*zdudif);
      testfn : real := (old fn[j,i]) + dfn;
      retfxsum, retfysum, retmsum, retfn, retm : real :=
        if (testfn < 0.0) then
          0.0, 0.0, 0.0, 0.0, 0.0
        else
          let
            % Calculate moment
            theta : real :=
              (ddvdif*zdudif - ddudif*zdvdif)*rd;
            dm : real := -aks *(allgamma[j] + allgamma[i] - theta);
            mji : real := old m[j,i] + dm;
            % Calculate shear force
            testft : real := mji*rr;
            % Is slip occurring
            ff : real := mu * testfn;
            abft : real := abs(testft);
            ft : real :=

```

```

        if (abft > ff) then ff * testft / abft
        else testft
        end if;
    retmji := r*ft;
    % Calculate force components (fx,fy)
    fx : real := (testfn*zdudif) - (ft*zdvdif);
    fy : real := (testfn*zdvdif) + (ft*zdudif);
    in
        fx, fy, retmji, testfn, retmji
    end let
    end if;
in
    retfxsum, retfysum, retmsum, retfn, retm
end let
end if;
returns
    value of sum fxsumji
    value of sum fysumji
    value of sum msumji
    array of fnji
    array of mji
end for;
returns
    array of fxsumji
    array of fysumji
    array of msumji
    array of fnji
    array of mji
end for;

%
% Now integrate accelerations to find displacements
%
u,v,w,ddu,ddv,gamma,du,dv:=
for j in 1, ncyl
uj,vj,wj,dduj,ddvj,gammaj,duj,dvj:=
if j=1 then
((fxsumj[j]*rmass)*tdel) * rlpluscon1,
((fysumj[j]*rmass+g)*tdel) * rlpluscon1,
((msumj[j]*rmoi)*tdel) * rlpluscon1,
0.0,
0.0,
((msumj[j]*rmoi)*tdel) * rlpluscon1,
0.0,
0.0
else
let
tuj:real:=(old u[j]*(1.0-con1) + ((fxsumj[j]*rmass)*tdel))
*rpluscon1;
tvj:real:=(old v[j]*(1.0-con1) + ((fysumj[j]*rmass+g)*tdel))
*rpluscon1;
twj:real:=(old w[j]*(1.0-con1) + ((msumj[j]*rmoi)*tdel))
*rpluscon1;
tdduj:=tuj*tdel;
tddvj:=tvj*tdel;
tgammaj:=twj*tdel
in

```



```
        tuj,
        tvj,
        twj,
        tdduj,
        tddvj,
        tgammaj,
        old du[j] + tdduj,
        old dv[j] + tddvj
    end let
end if;
returns
array of uj
array of vj
array of wj
array of dduj
array of ddvj
array of gammaj
array of duj
array of dvj
end for;
    iter := old iter + 1;
    cylinders := for j in 1,ncyl
returns
    array of record dudv_rec[du:du[j]; dv:dv[j]]
    end for;
returns
    array of cylinders when (mod(iter,its) = 0)
end for % number of iterations
end function % main
```

APPENDIX C: Explicitly annotated DECYL in Pascal - Version 1

```

program decyl(input, output);
{Original by L.Lorig 1985 (visitor to CSIRO Geomechanics Melb.Australia)}
{Pascal version by G.K.Egan 1990
 Laboratory for Concurrent Computing Systems
 Swinburne Institute of Technology }

label
    999;

const
    ncyl = 500;
    iside = 100;
    nn = 501 {ncyl+1};
    frames = 1;

type
    lock = volatile char;
    barrierrec = volatile array[0..31] of integer;
    ptrbarrier = ^barrierrec;

var
    ip,procs,p,i,j,n:integer;
        rz,
        z,
        dfn,
        theta,
        dm,
        ft,
        abft,
        ff,
        fx,
        fy,
        dudif,
        dvdif,
        ddudif,
        dddvdif:real;

shared
    klock: lock;
    k: integer;
    init_barrier,
    acc_barrier:barrierrec;
    fn,
    m: array [1..nn, 1..nn] of real;
    fxsum,
    fysum,
    msum,
    u,
    v,
    w,
    du,
    dv,
    da,
    gamma,
    ddu,
    ddv: array [1..nn] of real;
    mass,
    rmass,

```

```

        mu,
        moi,
        rmoi,
        pi,
        rho,
        d,
        dsqr,
        rd,
        r,
        rr,
        g,
        akn,
        aks,
        frac,
        freq,
        alpha,
        conl,
        rlplusconl,
        dn,
        tdel:real;
        kount,
        ikount,
        ii,
        its: integer;

{DECLARE lock=volatile char; ptrbarrier=^integer}

procedure spinlock(var l:lock); nonpascal;

procedure spinunlock(var l:lock); nonpascal;

procedure fbarrier_init(var b:barrierrec;count:integer;var p:integer);
nonpascal;

procedure fbarrier(var b: barrierrec); nonpascal;

function fork:integer; nonpascal;

procedure wait(i:integer); nonpascal;

procedure exit(i:integer); nonpascal;

procedure new_barrier(var b:barrierrec;count:integer; var pid:integer);

begin
    fbarrier_init(b,count,pid);
end;

function nfork(nprocs:integer):integer;
var proc,child:integer;
begin
    child:=-1;
    proc:= nprocs - 1;
    while (child <> 0) and (proc > 0) do
        begin

```

```

        child:=fork;
        if child <> 0 then
            proc:=pred(proc);
        end;
        nfork:=proc
    end;

procedure njoin(id,nprocs:integer);
var j:integer;

begin
    if id = 0 then
        for j := 1 to (nprocs - 1) do
            wait(0)
        else
            exit(0)
    end;

begin
    pi := 4.0 * arctan(1.0);
    rho := 2000.0;
    d := 100.0;
    rd:= 1.0/d;
    dsqr:=sqr(d);
    r := d / 2.0;
    rr:=2.0/d;
    g := - 10.0;
    mu := 0.1;
    mass := rho * pi * r * r;
    rmass:=1.0/mass;
    moi := mass * sqr(r) / 2.0;
    rmoi:=1.0/moi;
    akn := 1.0e9;
    aks := 1.0e9;
    frac := 1.00;
    freq := 0.200;
    alpha := 2.0 * pi * frac * freq;
    tdel := 2.0 * sqrt(mass / akn) / 10.0;
    conl := alpha * tdel / 2.0;
    r1plusconl:=1.0/(1.0+conl);
    {stack of cylinders}
    for i:=1 to ncyl do begin
        du[i]:=(i mod iside)*d;
        dv[i]:=(i/iside)*d+r;
    end;
    dv[nn] := - r;
    {Initialise forces, velocities etc.}
    for j := 1 to nn do
        begin
            for i := 1 to nn do
                begin
                    fn[j, i] := 0.0;
                    m[j, i] := 0.0;
                end;
            da[j] :=0.0;
            fxsum[j] := 0.0;
            fysum[j] := 0.0;
        end;
    end;
end;

```

```

    msum[j] := 0.0;
    u[j] := 0.0;
    v[j] := 0.0;
    w[j] := 0.0;
    ddu[j] := 0.0;
    ddv[j] := 0.0;
    gamma[j] := 0.0;
end;
its := 10;
ikount:=its div frames;
kount := ikount;
writeln(ncyl, ' ', its, ' ', frames);

writeln('procs ? ');
readln(procs);
new_barrier(init_barrier,procs,p);
new_barrier(acc_barrier,procs,p);

spinunlock(klock);

p:=nfork(procs);

for n := 1 to its do
begin {Loop over cylinders}
  if p = 0 then begin
    if kount = ikount then
      begin
        (for j:= 1 to ncyl do
          writeln(n-1, ' ', r, ' ', du[j], ' ', dv[j], ' ', da[j]);)
        kount := 0;
      end;
    kount := kount + 1;
  end;
  for j:= 1 to ncyl do
    begin {Place (ncyc+1)th cylinder 'opposite' jth}
      if p=0 then begin
        du[nn] := du[j];
        {Set gamma for (ncyc+1)th so get no shear interaction between
          jth cylinder and flat plane if former is rolling rather than
          sliding}
        gamma[nn] := - ddu[j] / r;
        {Look for interactions with cylinders with higher numbers}
        k := j + 1;
      end;

      fbarrier(init_barrier) {to protect k} ;

      repeat
        spinlock(klock);
        ip:=k;
        k:=k+1;
        spinunlock(klock);

        if ip <= nn then begin
          dudif := du[j] - du[ip];
          dvdif := dv[j] - dv[ip];
          {is the cylinder [ip] touching cylinder [j] ?}

```

```

z := dudif * dudif + dvdif * dvdif;
if z <= dsqr
then
begin
  rz := 1.0/sqrt(z);
  dudif := dudif * rz;
  dvdif := dvdif * rz;
  ddudif := ddu[ip] - ddu[j];
  ddvdif := ddv[ip] - ddv[j];
  {calculate the normal force fn[j,ip]}
  dfn := akn * (ddvdif * dvdif + ddudif * dudif);
  fn[j, ip] := fn[j, ip] + dfn;
  if fn[j, ip] >= 0.0
  then
begin
  {calculate moment}
  theta := (ddvdif * dudif - ddudif * dvdif) * rd;
  dm := - aks * (gamma[j] + gamma[ip] - theta);
  m[j, ip] := m[j, ip] + dm;
  {calculate shear force}
  ft := m[j, ip] * rr;
  {is slip occurring?}
  abft := abs(ft);
  ff := mu * fn[j, ip];
  if abft > ff then
    ft := ff * ft / abft;
  m[j, ip] := r * ft;
  {calculate force components (fx,fy)}
  fx := fn[j, ip] * dudif - ft * dvdif;
  fy := fn[j, ip] * dvdif + ft * dudif;
  {forces on cylinder j}
  fxsum[j] := fxsum[j] + fx;
  fysum[j] := fysum[j] + fy;
  msum[j] := msum[j] + m[j, ip];
  {reactions back on cylinder j}
  fxsum[ip] := fxsum[ip] - fx;
  fysum[ip] := fysum[ip] - fy;
  msum[ip] := msum[ip] + m[j, ip];
end
else
begin
  fn[j, ip] := 0.0;
  m[j, ip] := 0.0;
end
end
end
else
begin
  fn[j, ip] := 0.0;
  m[j, ip] := 0.0;
end;
end;
until ip>= nn;
{integrate accelerations to find displacements}
fbarrier(acc_barrier);
if p = 0 then begin
u[j] := (u[j] * (1.0 - conl) + ((fxsum[j] * rmass) * tdel)) *
        rlplusconl;

```

```
v[j] := (v[j] * (1.0 - con1) + ((fysum[j] * rmass + g) * tdel)) *
      rlpluscon1;
w[j] := (w[j] * (1.0 - con1) + ((msum[j] * rmoi) * tdel)) *
      rlpluscon1;

ddu[j] := u[j] * tdel;
ddv[j] := v[j] * tdel;
gamma[j] := w[j] * tdel;
du[j] := du[j] + ddu[j];
dv[j] := dv[j] + ddv[j];
da[j] := da[j] + gamma[j];
fxsum[j] := 0.0;
fysum[j] := 0.0;
msum[j] := 0.0;
end;
end;
writeln('finished ',p:1);
njoin(p,procs);
999:
end.
```

APPENDIX D: Explicitly annotated DECYL in Pascal - Version 2

```

program decyl(input, output);
{original by L.Lorig 1985 (visitor to CSIRO Geomechanics Melb.Australia)}
{translated to Pascal by G.K.Egan 1989
 Laboratory for Concurrent Computing Systems
 Swinburne Institute of Technology }

label
    999;

const
    ncyl = 500;
    iside = 100;
    nn = 501 {ncyl+1};
    frames = 1;

type
    lock = volatile char;
    barrierrec = volatile array[0..31] of integer;
    ptrbarrier = ^barrierrec;

var
    procs,p,i,j,k,n:integer;
        rz,
        z,
        dfn,
        gammann,
        dunn,
        theta,
        dm,
        ft,
        abft,
        ff,
        fx,
        fy,
        dudif,
        dvdif,
        ddudif,
        ddvdif:real;

shared
    acclock,jlock: lock;
    jj_global,
    j_global: integer;
    init_barrier,
    end_acc_barrier,
    acc_barrier:barrierrec;
    fn,
    m: array [1..nn, 1..nn] of real;
    fxsum,
    fysum,
    msum,
    u,
    v,
    w,
    du,
    dv,
    da,
    gamma,

```



```
        ddu,
        ddv: array [1..nn] of real;
        mass,
        rmass,
        mu,
        moi,
        rmoi,
        pi,
        rho,
        d,
        dsqr,
        rd,
        r,
        rr,
        g,
        akn,
        aks,
        frac,
        freq,
        alpha,
        con1,
        rlpluscon1,
        dn,
        tdel:real;
        kount,
        ikount,
        ii,
        its: integer;

{DECLARE lock=volatile char; ptrbarrier=^integer}

procedure spinlock(var l:lock); nonpascal;

procedure spinunlock(var l:lock); nonpascal;

procedure fbarrier_init(var b:barrierrec;count:integer;var p:integer);
nonpascal;

procedure fbarrier(var b: barrierrec); nonpascal;

function fork:integer; nonpascal;

procedure wait(i:integer); nonpascal;

procedure exit(i:integer); nonpascal;

procedure new_barrier(var b:barrierrec;count:integer; var pid:integer);

begin
    fbarrier_init(b,count,pid);
end;

function nfork(nprocs:integer):integer;
var proc,child:integer;
begin
```

```

child:=-1;
proc:= nprocs - 1;
while (child <> 0) and (proc > 0) do
  begin
    child:=fork;
    if child <> 0 then
      proc:=pred(proc);
    end;
    nfork:=proc
  end;

procedure njoin(id,nprocs:integer);
var j:integer;

begin
  if id = 0 then
    for j := 1 to (nprocs - 1) do
      wait(0)
    else
      exit(0)
  end;

begin
pi := 4.0 * arctan(1.0);
rho := 2000.0;
d := 100.0;
rd:= 1.0/d;
dsqr:=sqr(d);
r := d / 2.0;
rr:=2.0/d;
g := - 10.0;
mu := 0.1;
mass := rho * pi * r * r;
rmass:=1.0/mass;
moi := mass * sqr(r) / 2.0;
rmoi:=1.0/moi;
akn := 1.0e9;
aks := 1.0e9;
frac := 1.00;
freq := 0.200;
alpha := 2.0 * pi * frac * freq;
tdel := 2.0 * sqrt(mass / akn) / 10.0;
con1 := alpha * tdel / 2.0;
rlpluscon1:=1.0/(1.0+con1);
{stack of cylinders}
for i:=1 to ncy1 do begin
  du[i]:=(i mod iside)*d;
  dv[i]:=(i/iside)*d+r;
end;
dv[nn] := - r;
{Initialise forces, velocities etc.}
for j := 1 to nn do
  begin
    for i := 1 to nn do
      begin
        fn[j, i] := 0.0;
        m[j, i] := 0.0;

```

```

        end;
        da[j] :=0.0;
        fxsum[j] := 0.0;
        fysum[j] := 0.0;
        msum[j] := 0.0;
        u[j] := 0.0;
        v[j] := 0.0;
        w[j] := 0.0;
        ddu[j] := 0.0;
        ddv[j] := 0.0;
        gamma[j] := 0.0;
    end;
    its := 10;
    ikount:=its div frames;
    kount := ikount;
    writeln(ncyl, ' ', its, ' ', frames);

    writeln('procs ? ');
    readln(procs);
    new_barrier(init_barrier,procs,p);
    new_barrier(acc_barrier,procs,p);
    new_barrier(end_acc_barrier,procs,p);

    spinunlock(acclock);
    spinunlock(jlock);

    p:=nfork(procs);

    for n := 1 to its do
        begin {Loop over cylinders}
            if p = 0 then begin
                if kount = ikount then
                    begin
                        {for k:= 1 to ncyl do
                            writeln(n-1, ' ', r, ' ', du[k], ' ', dv[k], ' ', da[k]);}
                        kount := 0;
                    end;
                kount := kount + 1;
                j_global:=1;
                jj_global:=1
            end;

            fbarrier(init_barrier);

            repeat
                spinlock(jlock);
                j:=j_global;
                j_global:=j_global+1;
                spinunlock(jlock);

            if j <= ncyl then
                begin {Place (ncyc+1)th cylinder 'opposite' jth}
                    dunn := du[j];
                    {Set gamma for (ncyc+1)th so get no shear interaction between
                        jth cylinder and flat plane if former is rolling rather than
                        sliding}
                    gammann := - ddu[j] / r;

```

```

{Look for interactions with cylinders with higher numbers}
k := j + 1;

for i:= k to nn do begin
  if i = nn then
    dudif := du[j] - dunn
  else
    dudif := du[j] - du[i];
    dvdif := dv[j] - dv[i];
  {is the cylinder [i] touching cyclinder [j] ?}
  z := dudif * dudif + dvdif * dvdif;
  if z <= dsqr
  then
    begin
      rz := 1.0/sqrt(z);
      dudif := dudif * rz;
      dvdif := dvdif * rz;
      ddudif := ddu[i] - ddu[j];
      ddvdif := ddv[i] - ddv[j];
      {calculate the normal force fn[j,i]}
      dfn := akn * (ddvdif * dvdif + ddudif * dudif);
      fn[j, i] := fn[j, i] + dfn;
      if fn[j, i] >= 0.0
      then
        begin
          {calculate moment}
          theta := (ddvdif * dudif - ddudif * dvdif) * rd;
          if i = nn then
            dm := - aks * (gamma[j] + gammann - theta)
          else
            dm := - aks * (gamma[j] + gamma[i] - theta);
          m[j, i] := m[j, i] + dm;
          {calculate shear force}
          ft := m[j, i] * rr;
          {is sli occurring?}
          abft := abs(ft);
          ff := mu * fn[j, i];
          if abft > ff then
            ft := ff * ft / abft;
          m[j, i] := r * ft;
          {calculate force components (fx,fy)}
          fx := fn[j, i] * dudif - ft * dvdif;
          fy := fn[j, i] * dvdif + ft * dudif;
          {forces on cylinder j}
          fxsum[j] := fxsum[j] + fx;
          fysum[j] := fysum[j] + fy;
          msum[j] := msum[j] + m[j, i];
          {reactions back on cylinder j}
          spinlock(accllock);
          fxsum[i] := fxsum[i] - fx;
          fysum[i] := fysum[i] - fy;
          msum[i] := msum[i] + m[j, i];
          spinunlock(accllock);
        end
      else
        begin
          fn[j, i] := 0.0;
        end
    end
  end
end

```

```

                m[j, i] := 0.0;
            end
        end
    else
        begin
            fn[j, i] := 0.0;
            m[j, i] := 0.0;
        end;
    end;
end;
end;
{integrate accelerations to find displacements}
until j>= nn;

fbarrier(acc_barrier);

repeat
    spinlock(jlock);
    j:=jj_global;
    jj_global:=jj_global+1;
    spinunlock(jlock);

    if j <= ncyl then begin
        u[j] := (u[j] * (1.0 - con1) + ((fxsum[j] * rmass) * tdel)) *
rlpluscon1;
        v[j] := (v[j] * (1.0 - con1) + ((fysum[j] * rmass + g) * tdel)) *
rlplusc
on1;
        w[j] := (w[j] * (1.0 - con1) + ((msum[j] * rmoi) * tdel)) *
rlpluscon1;
        ddu[j] := u[j] * tdel;
        ddv[j] := v[j] * tdel;
        gamma[j] := w[j] * tdel;
        du[j] := du[j] + ddu[j];
        dv[j] := dv[j] + ddv[j];
        da[j]:=da[j]+gamma[j];
        fxsum[j] := 0.0;
        fysum[j] := 0.0;
        msum[j] := 0.0;
    end;
until j>= ncyl;
fbarrier(end_acc_barrier);
end;
writeln('finished ',p:1);
njoin(p,procs);
999:
end.

```